

**Q.1(a) Test whether  $P(s) = s^5 + 12s^4 + 45s^3 + 60s^2 + 44s + 48$  is Hurwitz [5] polynomial.**

**(A)**  $P(s) = s^5 + 12s^4 + 45s^3 + 60s^2 + 44s + 48$

$s^5$	1	45	44
$s^4$	12	60	48
$s^3$	40	40	0
$s^2$	48	48	
$s^1$	0	0	

As complete row becomes zero we will form an auxiliary equation.

$$A(s) = 48s^2 + 48$$

$$A'(s) = 96s + 0$$

Replacing zero<sup>th</sup> row with  $A'(s)$

$s^5$	1	45	44
$s^4$	12	60	48
$s^3$	40	40	0
$s^2$	48	48	
$s^1$	96	0	
$s^0$	48		

As all the elements in the 1<sup>st</sup> columns are positive given  $f^n$  is a Hurwitz polynomial.

**Q.1(b) The constants of a transmission line are  $R = 6 \Omega/\text{km}$ , [5]  
 $L = 2.2 \text{ mH}/\text{km}$ ,  $G = 0.25 \times 10^{-6} \text{ } \Omega/\text{km}$ ,  $C = 0.005 \times 10^{-5} \text{ F}/\text{km}$ .  
Determine the characteristic impedance, propagation constant and attenuation constant at 1 KHz.**

**(A)** Given :  $R = 6 \Omega / \text{km}$ ,  $L = 2.2 \text{ mH}/\text{km}$ ,  $G = 0.25 \times 10^{-6} \text{ } \Omega / \text{km}$   
 $C = 0.005 \times 10^{-5} \text{ F}/\text{km}$ ,  $F = 1\text{KHz}$

To find :  $Z_0, \gamma, \alpha$

$$\begin{aligned} z &= R + j\omega L \\ &= 6 + j2\pi \times 10^3 \times 2.2 \times 10^{-3} \\ &= 6 + j13.82 \\ z &= 15.06 \angle 66.53^\circ \end{aligned}$$

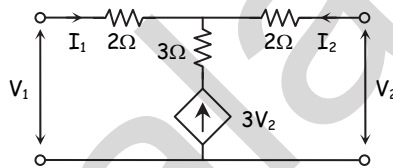
$$\begin{aligned}
 y &= G + j\omega C \\
 &= 0.25 \times 10^{-6} + j2\pi 10^3 \times 0.005 \times 10^{-5} \\
 &= 0.25 \times 10^{-6} + j 3.14 \times 10^{-4} \\
 &= 3.14 \times 10^{-4} \angle 89.95^\circ
 \end{aligned}$$

$$\begin{aligned}
 \text{Characteristic impedance} = z_0 &= \sqrt{\frac{z}{y}} = \sqrt{\frac{15.06 \angle 66.53^\circ}{3.14 \times 10^{-4} \angle 89.95^\circ}} \\
 &= 219.00 \angle 11.71^\circ \Omega
 \end{aligned}$$

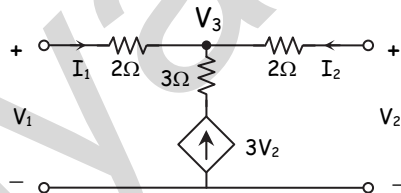
Propagation constant

$$\begin{aligned}
 \gamma &= \sqrt{z \cdot y} = \sqrt{(15.06 \angle 66.53)(3.14 \times 10^{-4} \angle 89.95)} \\
 \gamma &= 0.014 + j 0.067 / \text{km} \\
 \gamma &= \alpha + j\beta \\
 \alpha &= 0.014 \text{ Np/km,} \\
 \beta &= 0.067 \text{ rad/km}
 \end{aligned}$$

Q.1(c) Determine the short circuit admittance parameters of the network [5]  
shown :



(A)



Apply RCL at  $V_3$

$$\frac{V_3 - V_1}{2} + \frac{V_3 - V_2}{2} = 3V_2$$

$$V_3 \left( \frac{1}{2} + \frac{1}{2} \right) = 3V_2 + \frac{V_2}{2} + \frac{V_1}{2}$$

$$V_3 = 0.5 V_1 + 3.5 V_2$$

...(1)

Apply KCL at  $V_1$

$$I_1 = \frac{V_1 - V_3}{2}$$

$$I_1 = \frac{V_1}{2} = \frac{1}{2} (0.5V_1 + 3.5V_2)$$

$$I_1 = V_1 (0.25) - V_2 (1.75)$$

Comparing with  $I_1 = y_{11}V_1 + y_{12} V_2$

$$y_{11} = 0.25 \text{ } \bar{\Omega} \quad y_{12} = -1.75 \bar{\Omega}$$

Apply KCL at  $V_2$

$$I_2 = \frac{V_2 - V_3}{2}$$

$$I_2 = \frac{V_2}{2} - \frac{1}{2}(0.5V_1 + 3.5V_2)$$

$$I_2 = -0.25 V_1 - 1.25 V_2$$

$$y_{21} = -0.25 \bar{\Omega}, \quad y_{22} = -1.25 \bar{\Omega}$$

**Q.1(d)** State and prove final value theorem of Laplace transform.

[5]

**(A)** If  $L\{f(t)\} = F(s)$  then  $\lim_{t \rightarrow \infty} f(t) = \lim_{s \rightarrow 0} sF(s)$

Proof : We know that

$$L\{f'(t)\} = sF(s) - f(0)$$

$$sF(s) = L\{f'(t)\} + f(0)$$

$$sF(s) = \lim_{s \rightarrow 0} \int_0^{\infty} f'(t)e^{-st} dt + f(0)$$

$$= \int_0^{\infty} \lim_{s \rightarrow 0} [f'(t)e^{-st}] dt + f(0)$$

$$= \int_0^{\infty} f'(t) dt + f(0)$$

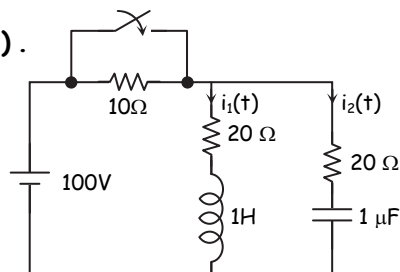
$$= [f(t)]_0^{\infty} + f(0)$$

$$= \lim_{t \rightarrow \infty} f(t) - f(0) + f(0)$$

$$= \lim_{t \rightarrow \infty} f(t)$$

**Q.2(a)** The network shown in figure, a steady state is reached with the switch open. At  $t = 0$ , the switch is closed. Determine  $V_c(0^-)$ ,

$i_1(0^+)$ ,  $i_2(0^+)$ ,  $\frac{di_1}{dt}(0^+)$  and  $\frac{di_2}{dt}(0^+)$ .



**(A) Step 1:** At  $t = 0^-$ , switch is open  
 $i_2(0^-) = 0$

finding  $i_1(0^-)$

$$100 - 10 i_1 - 20 i_1 = 0$$

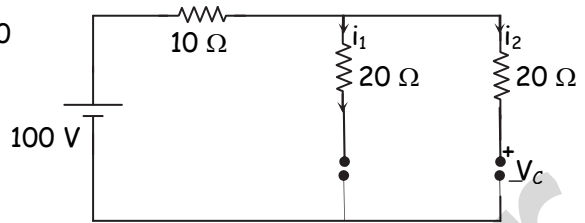
$$100 = 30 i_1$$

$$\therefore i_1 = \frac{100}{30} = \frac{10}{3} \text{ A}$$

$$\therefore i_1(0^-) = \frac{10}{3} \text{ A}$$

$$V_C(0^-) = 20 \times i_1(0^-) = 20 \times \frac{10}{3}$$

$$V_C(0^-) = \frac{200}{3} \text{ V}$$



**Step 2:** At  $t = 0^+$

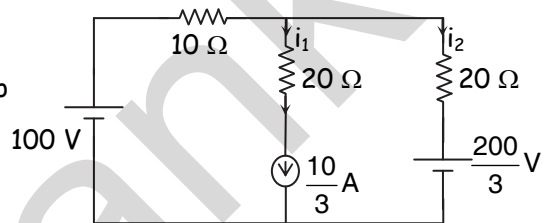
$$i_1(0^+) = \frac{10}{3} \text{ A}$$

Apply KVL to the outer loop

$$100 - 20i_2 - \frac{200}{3} = 0$$

$$20 i_2 = 100 - \frac{200}{3}$$

$$i_2(0^+) = 1.67 \text{ A}$$



**Step 3:** At  $t > 0$

Apply KVL to loop (1)

$$100 - 20 i_1 - \frac{di_1}{dt} = 0$$

$$\frac{di_1}{dt} = 100 - 20 i_1(0^+)$$

$$= 100 - \frac{20 \times 10}{3}$$

$$\frac{di_1}{dt} = 33.33 \text{ A/s}$$

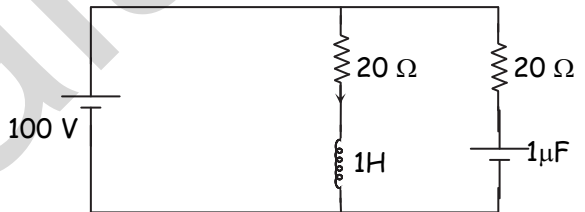
Apply KVL to outer loop

$$100 - 20 i_2 - \frac{1}{10^{-6}} \int i_2 dt = 0$$

Differentiate w.r.t.  $t$

$$0 - 20 \frac{di_2}{dt} - 10^6 i_2 = 0$$

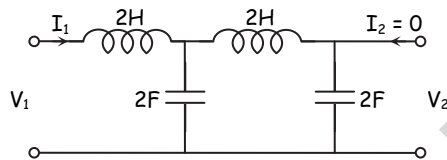
$$-20 \frac{di_2(0^+)}{dt} = 10^6 i_2(0^+)$$



$$\frac{di_2}{dt} = \frac{-10^6(1.67)}{20}$$

$$\frac{di_2}{dt} = -83500 \text{ A/s}$$

Q.2(b) Find the network functions  $\frac{V_1}{I_1}, \frac{V_2}{I_1}, \frac{V_2}{V_1}$  for the network shown : [5]



(A) Let  $V_2 = 1$

$$I_b = V_2 \times 2S$$

$$V_a = V_2 + I_b \cdot 2S \\ = 1 + 2S \cdot 2S$$

$$V_a = 1 + 4S^2$$

$$I_a = V_a \cdot 2S \\ = (1 + 4S^2) \cdot 2S$$

$$I_a = 2S + 8S^3$$

$$I_1 = I_a + I_b \\ = 2S + 8S^3 + 2S$$

$$I_1 = 8S^3 + 4S$$

$$V_1 = V_a + I_1 \cdot 2S \\ = 1 + 4S^2 + (8S^3 + 4S) \cdot 2S \\ = 1 + 4S^2 + 16S^4 + 8S^2$$

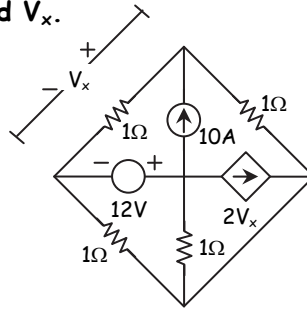
$$V_1 = 16S^4 + 12S^2 + 1$$

$$\frac{V_1}{I_1} = \frac{16S^4 + 12S^2 + 1}{8S^3 + 4S}$$

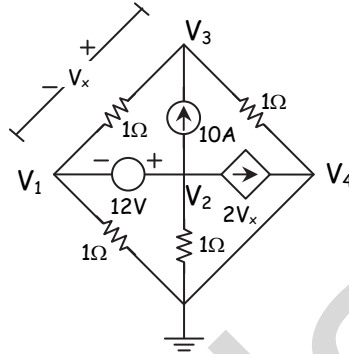
$$\frac{V_2}{I_1} = \frac{1}{8S^3 + 4S} \quad \& \quad \frac{V_2}{V_1} = \frac{1}{16S^4 + 12S^2 + 1}$$

Q.2(c) In the circuit shown in figure, find  $V_x$ .

[5]



(A)



$$V_4 = 0 \text{ V}$$

$$V_x = V_1 - V_3 \quad \dots(1)$$

Relation between  $V_1$  &  $V_2$

$$V_2 - V_1 = 12$$

$$-V_1 + V_2 + 0V_3 = 12 \quad \dots(2)$$

Supernode equation

$$\frac{V_1 - V_3}{1} + \frac{V_1}{1} + \frac{V_2}{1} + 10 + 2V_x = 0$$

$$V_1 - V_3 + V_1 + V_2 + 10 + 2(V_1 - V_3) = 0 \quad \dots(\text{from 1})$$

$$4V_1 + V_2 - 3V_3 = -10 \quad \dots(3)$$

KCL to  $V_3$

$$\frac{V_3 - V_1}{1} + \frac{V_3}{1} = 10$$

$$-V_1 + 0V_2 + 2V_3 = 10 \quad \dots(4)$$

Solving (2), (3) & (4)

$$V_1 = -2 \text{ V}$$

$$V_2 = 10 \text{ V}$$

$$V_3 = 4 \text{ V}$$

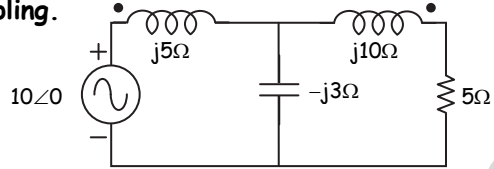
$$V_x = V_1 - V_3$$

$$V_x = -2 - 4$$

$$V_x = -6 \text{ V}$$

Q.3(a) Find the voltage across  $5 \Omega$  resistor in the network shown below. [8]

If  $K = 0.8$  is coefficient of coupling.

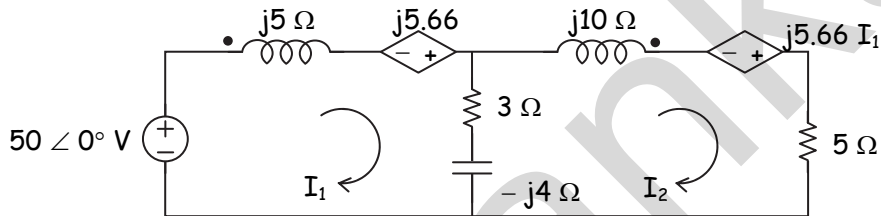


(A) For a magnetically coupled circuit,

$$M = K\sqrt{5(10)}$$

$$X_m = K\sqrt{X_{L_1} X_{L_2}} = 0.8\sqrt{5(10)} = 5.66 \Omega$$

The equivalent circuit in terms of dependent sources can be drawn as



Applying KVL to Mesh 1,

$$50 \angle 0^\circ - j5I_1 - 3(I_1 - I_2) + j4(I_1 - I_2) + j5.66I_2 = 0$$

$$50 \angle 0^\circ = (3 + j1) I_1 - (3 + j1.66) I_2 \quad \dots (1)$$

$$(3 + j1) I_2 + (-3 - j1.66) I_2 = 50 \angle 0^\circ$$

Applying KVL to Mesh 2,

$$j4(I_2 - I_1) - 3(I_2 - I_1) - j10I_2 + j5.66I_1 - 5I_2 = 0$$

$$j4 I_2 - j4I_1 - 3I_2 + 3I_1 - j10I_2 + j5.66I_1 - 5I_2 = 0$$

$$-j4 I_2 + j4I_1 + 3I_2 - 3I_1 + j10I_2 - j5.66I_1 + 5I_2 = 0$$

$$(-3 - j1.66) I_1 + (8 + j6) I_2 = 0 \quad \dots (2)$$

By Cramer's rule,

$$I_2 = \frac{\begin{vmatrix} 3 + j1 & 50 \angle 0^\circ \\ -3 - j1.66 & 0 \end{vmatrix}}{\begin{vmatrix} 3 + j1 & -3 - j1.66 \\ -3 - j1.66 & 8 + j6 \end{vmatrix}} = 8.62 \angle -24.79^\circ \text{ A}$$

$$V = 5I_2 = 5(8.62 \angle -24.79^\circ) = 43.1 \angle -24.79^\circ \text{ V}$$

Q.3(b) Check the positive real function :

[8]

$$(i) F(s) = \frac{s^2 + 6s + 5}{s^2 + 9s + 14} \quad (ii) F(s) = \frac{s^3 + 6s^2 + 7s + 3}{s^2 + 2s + 1}$$

$$(A) (i) F(s) = \frac{s^2 + 6s + 5}{s^2 + 9s + 14}$$

$$\text{Step 1 : Let } F(s) = \frac{N(s)}{D(s)} = \frac{s^2 + 6s + 5}{s^2 + 9s + 14}$$

$$F(s) = \frac{(s+5)(s+1)}{(s+7)(s+2)}$$

The function  $f(s)$  has poles at  $s = -7$  &  $s = -2$  & zeros at  $s = -5$  and  $s = -1$   
 $\therefore$  All the poles & zeros are in the left half of  $s$ -plane.

**Step 2 :** As there is no pole on  $jw$  axis, the residue test is not carried out.

**Step 3 :** Even part of  $N(s) = m_1 = s^2 + 5$

Odd part of  $N(s) = n_1 = 6s$

Even part of  $D(s) = m_2 = s^2 + 14$

Odd part of  $D(s) = n_2 = 9s$

$$A(w^2) = m_1 m_2 - n_1 n_2 = (s^2 + 5)(s^2 + 14) - (6s)(9s) \Big|_{s=jw}$$

$$= s^4 - 35s^2 + 70 \Big|_{s=jw}$$

$$\therefore A(w^2) = w^4 + 35w^2 + 70$$

$A(w^2)$  is positive for all  $w \geq 0$

As all the three conditions are satisfied, the function is a positive real function.

$$(ii) F(s) = \frac{s^3 + 6s^2 + 7s + 3}{s^2 + 2s + 1}$$

$$\text{Step 1 : Let } F(s) = \frac{N(s)}{D(s)} = \frac{s^3 + 6s^2 + 7s + 3}{s^2 + 2s + 1}$$

$$F(s) = \frac{s^3 + 6s^2 + 7s + 3}{(s+1)^2}$$

From above both the poles are lying at  $s = -1$

Now we will check for  $N(s)$

$$N(s) = s^3 + 6s^2 + 7s + 3$$

The Routh array of  $N(s)$  is given by

$s^3$	1	7
$s^2$	6	3
$s^1$	$\frac{39}{6}$	0
$s^0$	3	

As all elements in 1<sup>st</sup> column are +ve,  $N(s)$  is Hurwitz polynomial.

$\therefore$  1<sup>st</sup> condition is satisfied.



**Step 2 :** As there is no pole on  $jw$  axis, residue test need not to be carried out.

**Step 3 :** Even part of  $N(s) = m_1 = 6s^2 + 3$

Odd part of  $N(s) = n_1 = s^3 + 7s$

Even part of  $D(s) = m_2 = s^2 + 1$

Odd part of  $D(s) = n_2 = 2s$

$$\begin{aligned} A(w^2) &= m_1 m_2 - n_1 n_2 \\ &= (6s^2 + 3)(s^2 + 1) - (s^3 + 7s)(2s) \Big|_{s=jw} \\ &= 4s^4 - 5s^2 + 3 \Big|_{s=jw} \end{aligned}$$

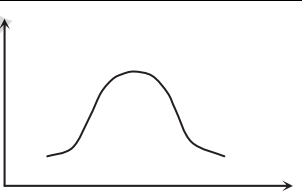
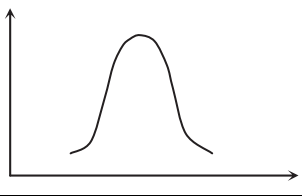
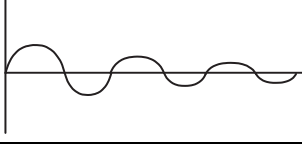
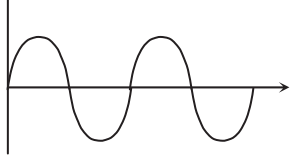
$$A(w^2) = 4w^4 + 5w^2 + 3$$

$\therefore$  We can say that  $A(w^2)$  is positive for all  $w \geq 0$

As all three conditions are satisfied, function  $f(s)$  is a positive real function.

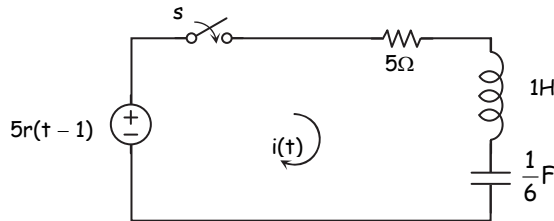
**Q.3(c) List the types of damping in series R-L-C circuit and mention the condition for each damping. [4]**

(A)

	Nature of Roots	System	Response
1.	Negative unequal Real	Over damped $k_1 e^{p_1 t} + k_2 e^{p_2 t}$	
2.	Negative Real equal	Critically damped $k_1 e^{pt} + k_2 t e^{pt}$	
3.	Complex conjugate	Underdamped $e^{-\alpha t} [k_1 \cos \omega t + k_2 \sin \omega t]$	
4.	Conjugate imaginary	Oscillatory $k_1 \cos \omega t + k_2 \sin \omega t$	

where  $\alpha = \frac{R}{2L}$  and  $\omega_0 = \frac{1}{\sqrt{LC}}$

Q.4(a) For the network shown, determine the current  $i(t)$  when the switch is closed at  $t = 0$  with zero initial conditions. [8]

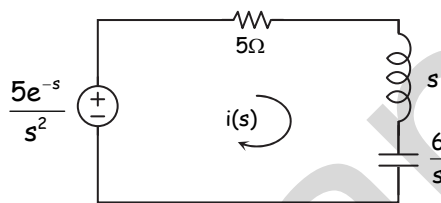


(A) Step 1 At  $t = 0^-$ , switch is open

$$i(0^-) = 0 \text{ A}$$

$$V_c(0^-) = 0 \text{ V}$$

Step 2 At  $t > 0$ , switch is closed.



Applying KVL

$$5 \frac{e^{-s}}{s^2} - 5i(s) - si(s) - \frac{6}{s}i(s) = 0$$

$$\frac{5e^{-s}}{s^2} = i(s) \left( 5 + s + \frac{6}{s} \right)$$

$$\frac{5e^{-s}}{s^2} = \frac{5s + s^2 + 6}{s} i(s)$$

$$(s^2 + 5s + 6) i(s) = \frac{5e^{-s}}{s}$$

$$i(s) = \frac{5e^{-s}}{s(s^2 + 5s + 6)}$$

$$i(s) = \frac{5e^{-s}}{s(s+3)(s+2)}$$

$$\text{Let } i_1(s) = \frac{1}{s(s+3)(s+2)} = \frac{A}{s} + \frac{B}{s+3} + \frac{C}{s+2}$$

$$1 = A(s+3)(s+2) + Bs(s+2) + Cs(s+3)$$

$$A = \frac{1}{6}, \quad B = \frac{1}{3}, \quad C = -\frac{1}{2}$$

$$i(C) = 5e^{-s} \times i_1(s)$$

$$= 5e^{-s} \left[ \frac{1}{6s} + \frac{1}{3(s+3)} - \frac{1}{2(s+2)} \right]$$

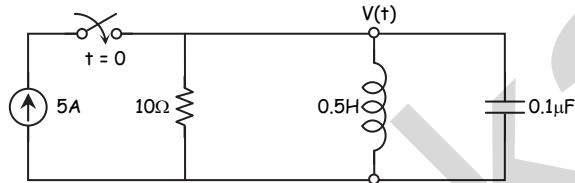
$$i(s) = \frac{5e^{-s}}{6s} + \frac{5e^{-s}}{3(s+3)} - \frac{5e^{-s}}{2(s+2)}$$

Taking inverse laplace transform

$$i(t) = \frac{5}{6}u(t-1) + \frac{5}{3}e^{-3(t-1)}u(t-1) - \frac{5}{2}e^{-2(t-1)}u(t-1)$$

Q.4(b) In the given network switch is closed at  $t = 0$ . Solve for  $V$ ,  $\frac{dV}{dt}$ , [8]

$$\frac{d^2V}{dt^2} \text{ at } t = 0^+$$

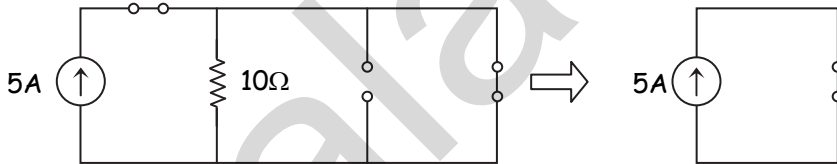


(A) Step 1 : At  $t = 0^-$ , switch is open.

$$i_L(0^-) = 0 \text{ A}$$

$$V_c(0^-) = 0V \text{ \& } V(0^-) = 0V$$

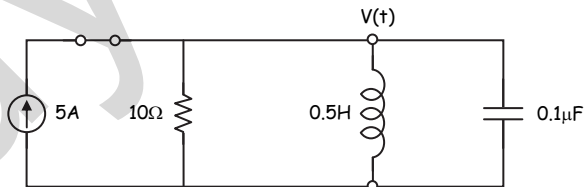
Step 2: At  $t = 0^+$ , switch is closed.



$$i_L(0^+) = 0A$$

$$V_1(0^+) = 0V, \quad V(0^+) = 0V$$

Step 3: At  $t > 0$



Applying KCL to  $V$

$$\frac{V}{10} + \frac{1}{0.5} \int V dt + 0.1 \times 10^{-6} \frac{dV}{dt} = 5 \quad \dots(1)$$

At  $t = 0^+$

$$\frac{V(0^+)}{10} + 0 + 0.1 \times 10^{-6} \frac{dV}{dt}(0^+) = 5$$

$$0.1 \times 10^{-6} \frac{dV}{dt}(0^+) = 5 - 0$$

$$\frac{dV}{dt}(0^+) = \frac{5}{0.1 \times 10^{-6}}$$

$$\frac{dV}{dt}(0^+) = 50 \times 10^{12} \text{ v/s}$$

Diff. equation (1) w.r.t. t

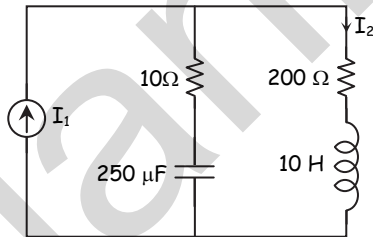
$$\frac{dV}{10 dt} + \frac{1}{0.5} V(0^+) + 0.1 \times 10^{-6} \frac{d^2V}{dt^2} = 0$$

$$0.1 \times 10^{-6} \frac{d^2V}{dt^2} = \frac{-dV}{10 dt}$$

$$\frac{d^2V}{dt^2} = -\frac{50 \times 10^6}{10 \times 0.1 \times 10^{-6}}$$

$$\frac{d^2V}{dt^2} = -50 \times 10^{12} \text{ V/s}^2$$

Q.4(c) Obtain pole-zero plot for  $\frac{I_2}{I_1}$ .



[4]

(A) By C.D.R.

$$I_2 = \frac{\frac{4000}{s} + 10}{\frac{4000}{s} + 10 + 200 + 10s} \times I_1$$

$$\frac{I_2}{I_1} = \frac{\frac{4000 + 10s}{s}}{\frac{4000 + 10s + 200s + 10s^2}{s}}$$

$$\frac{I_2}{I_1} = \frac{4000 + 10s}{10s^2 + 210s + 4000}$$

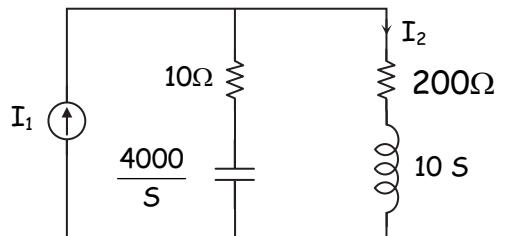
$$\frac{I_2}{I_1} = \frac{10(s + 400)}{10(s^2 + 21s + 400)}$$

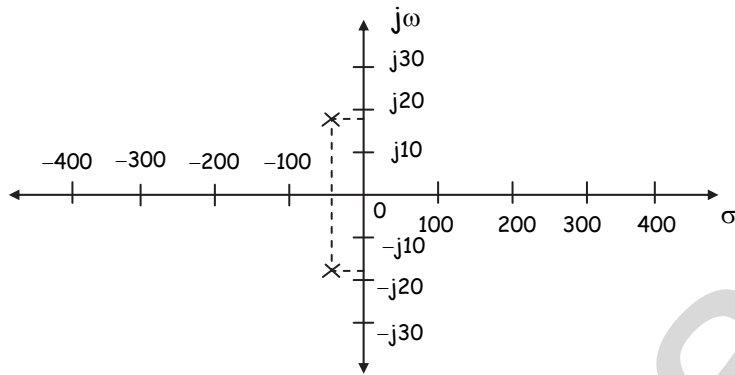
$$\frac{I_2}{I_1} = \frac{s + 400}{s^2 + 21s + 400}$$

$$Z_1 = -400$$

$$P_1 = -10.5 + 17.02j$$

$$P_2 = -10.5 - 17.02j$$





Q.5(a) Synthesize the driving point function using Foster-I and Foster-II [10]

form :  $Z(s) = \frac{2(s^2 + 1)(s^2 + 9)}{s(s^2 + 4)}$

(A) Foster – I form :

A degree of numerator is greater than degree of denominator, division is first carried out.

$$Z(s) = \frac{4(s^2 + 1)(s^2 + 9)}{s(s^2 + 4)} = \frac{4s^4 + 40s^2 + 36}{s^3 + 4s}$$

$$\begin{array}{r} 4s \\ s^3 + 4s \overline{) 4s^4 + 40s^2 + 36} \\ \underline{4s^4 + 16s^2} \phantom{+ 36} \\ 24s^2 + 36 \end{array}$$

$$\therefore Z(s) = \text{Quotient} + \frac{\text{Remainder}}{\text{Diviser}} = 4s + \frac{24s^2 + 36}{s^3 + 4s} = 4s + \frac{24s^2 + 36}{s(s^2 + 4)}$$

By partial fraction expansion

$$Z(s) = 4s + \frac{k_0}{s} + \frac{2k_1 s}{s^2 + 4}$$

$$k_0 = sz(s) \Big|_{s=0} = \frac{4(1)(9)}{4} = 9$$

$$k_1 = \frac{(s^2 + 4)z(s)}{2s} \Big|_{s^2=-4} = \frac{4(-4+1)(-4+9)}{2(-4)} = \frac{15}{2}$$

$$Z(s) = 4s + \frac{9}{s} + \frac{15s}{s^2 + 4}$$

1<sup>st</sup> term  $\Rightarrow 4s \Rightarrow$  inductor of 4H

2<sup>nd</sup> term  $\Rightarrow \frac{9}{s} \Rightarrow$  capacitor of  $\frac{1}{9}$ F

3<sup>rd</sup> term  $\Rightarrow$  parallel LC network

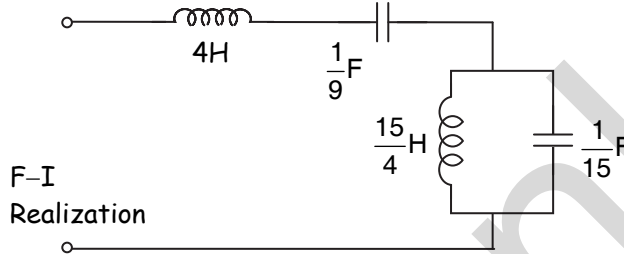
For parallel LC network

$$Z_{LC}(s) = \frac{\left(\frac{1}{C}\right)_s}{s^2 + \frac{1}{LC}}$$

Comparing the terms

$$\therefore C = \frac{1}{15} \text{ F and } L = \frac{15}{4} \text{ H}$$

\(\therefore\) Corresponding network is as follows.



**Foster II form :**

It is obtain by partial fraction expansion of admittance function

$$Y(s) = \frac{s(s^2 + 4)}{4(s^2 + 1)(s^2 + 9)}$$

By partial fraction expansion

$$Y(s) = \frac{2k_1 s}{s^2 + 1} + \frac{2k_2 s}{s^2 + 9}$$

$$k_1 = \frac{(s^2 + 1)}{2s} Y(s) \Big|_{s^2 = -1} = \frac{(-1 + 4)}{8(-1 + 9)} = \frac{3}{64}$$

$$k_2 = \frac{s^2 + 9}{2s} Y(s) \Big|_{s^2 = -9} = \frac{(-9 + 4)}{8(-9 + 1)} = \frac{5}{64}$$

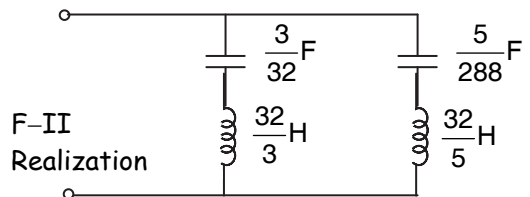
$$Y(s) = \frac{\left(\frac{3}{32}\right)s}{s^2 + 1} + \frac{\left(\frac{5}{32}\right)s}{s^2 + 9}$$

Above two terms presents admittance of series LC network for series LC

$$\text{network} \Rightarrow Y_{LC}(s) = \frac{\left(\frac{1}{L}\right)_s}{s^2 + \frac{1}{LC}}$$

\(\therefore\) By comparison

$$L_1 = \frac{3L}{3} \text{ H} \quad C_1 = \frac{3}{32} \text{ F}$$

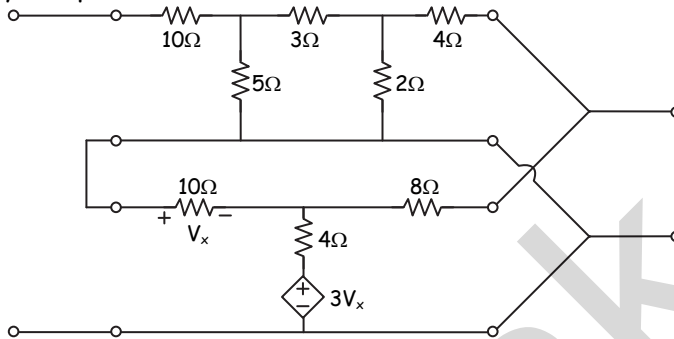


$$L_2 = \frac{32}{5} \text{H} \quad C_2 = \frac{5}{288} \text{F}$$

Corresponding network is as shown.

Q.5(b) Obtain hybrid parameter of the inter-connected network.

[10]



(A) Separate the two networks

1<sup>st</sup> network

$$V_x = 10 I_1$$

Apply KVL to loop of  $I_1$

$$V_1 - 10I_1 - 4(I_1 + I_2) - 3V_x = 0$$

$$V_1 = 10 I_1 + 4(I_1 + I_2) + 3(10I_1)$$

$$V_1 = 10I_1 + 4I_1 + 4I_2 + 30I_1$$

$$V_1 = 44I_1 + 4I_2$$

Comparing with  $V_1 = z_{11} I_1 + z_{12}I_2$

$$\therefore z_{11} = 44\Omega \quad z_{12} = 4\Omega$$

Apply KVL to loop of  $I_2$

$$V_2 - 8I_2 - 4(I_2 + I_1) - 3V_x = 0$$

$$V_2 = 8I_2 + 4(I_2 + I_1) + 3(10I_1)$$

$$V_2 = 34I_1 + 12I_2$$

Comparing with

$$V_2 = z_{21}I_1 + z_{22} I_2$$

$$\therefore z_{21} = 34 \Omega \quad z_{22} = 12\Omega$$

$$\Delta Z = z_{11} z_{22} - z_{21} z_{12} = 44 \times 12 - 34 \times 4$$

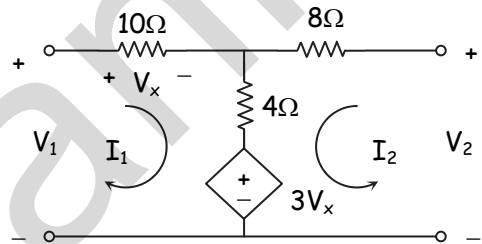
$$\Delta Z = 392$$

Now finding h-parameters from Z-parameter

$$h'_{11} = \frac{\Delta Z}{z_{22}} = \frac{392}{12} = 32.66$$

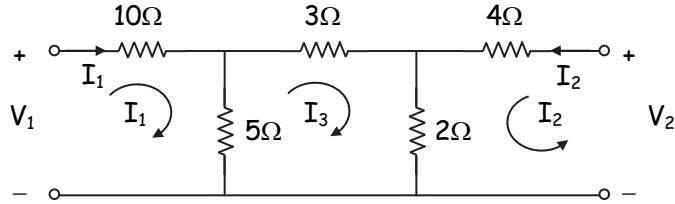
$$h''_{12} = \frac{z_{12}}{z_{22}} = \frac{4}{12} = 0.333$$

$$h'_{21} = \frac{-z_{21}}{z_{22}} = \frac{-34}{12} = -2.833$$



$$h'_{22} = \frac{1}{Z_{22}} = \frac{1}{12} = 0.0833$$

$$\therefore \begin{bmatrix} h'_{11} & h'_{12} \\ h'_{21} & h'_{22} \end{bmatrix} = \begin{bmatrix} 32.66 & 0.333 \\ -2.833 & 0.0833 \end{bmatrix}$$



Apply KVL to  $I_3$

$$-5(I_3 - I_1) - 3I_3 - 2(I_3 + I_2) = 0$$

$$-10I_3 + 5I_1 - 2I_2 = 0$$

$$I_3 = \frac{-5I_1 + 2I_2}{-10}$$

$$I_3 = 0.5 I_1 - 0.2 I_2 \quad \dots(1)$$

Apply KVL to  $I_1$

$$V_1 - 10I_1 - 5(I_1 - I_3) = 0$$

$$V_1 = 10I_1 + 5I_1 - 5(0.5I_1 - 0.2I_2)$$

$$V_1 = 12.5I_1 + I_2$$

$$\therefore Z_{11} = 12.5\Omega \text{ \& } Z_{12} = 1\Omega$$

Apply KVL to  $I_2$

$$V_2 - 4I_2 - 2(I_2 + I_3) = 0$$

$$V_2 = 4I_2 + 2I_2 + 2(0.5I_1 - 0.2I_2)$$

$$V_2 = I_1 + 5.6 I_2$$

$$\therefore Z_{21} = 1\Omega \quad Z_{22} = 5.6 \Omega$$

$$\Delta Z = Z_{11} Z_{22} - Z_{12} Z_{21} = 12.5 \times 5.6 - 1 \times 1 = 69$$

Converting Z to h parameters

$$\begin{bmatrix} h''_{11} & h''_{12} \\ h''_{21} & h''_{22} \end{bmatrix} = \begin{bmatrix} 12.32 & 0.178 \\ -0.178 & 0.178 \end{bmatrix}$$

h - parameter of the interconnected network is given by,

$$\begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} = \begin{bmatrix} h'_{11} + h''_{11} & h'_{12} + h''_{12} \\ h'_{21} + h''_{21} & h'_{22} + h''_{22} \end{bmatrix}$$

$$\begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} = \begin{bmatrix} 44.98 & 0.511 \\ -3.011 & 0.261 \end{bmatrix}$$



Q.6(a) The characteristic impedance of a high frequency line is  $100 \Omega$ . [10]  
 If its terminated by a load impedance of  $100 + j100\Omega$ . Using smith chart, find out : (i) VSWR, (ii) Reflection coefficient, (iii) Impedance at  $(1/10)^{\text{th}}$  of wave length away from load, (iv) VSWR minimum and VSWR maximum away from the load.

(A)  $Z_L = 100 + j100$

$$\bar{Z}_L = \frac{100 + j100}{100} = 1 + j1$$

i) VSWR = 2.6

ii) Reflection coefficient =  $0.44 \angle 64^\circ$

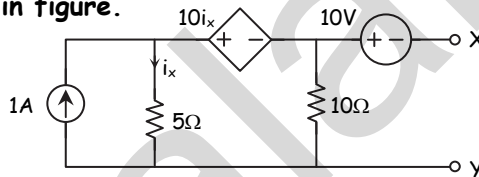
iii) Impedance at  $\frac{1}{10}^{\text{th}}$  of  $\lambda$  away from load =  $2.5 - j0.4$

iv) VSWR minimum =  $0.25 \lambda + 0.088 = 0.338 \lambda$

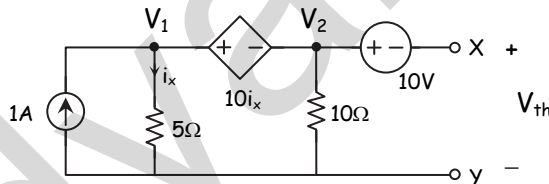
VSWR maximum =  $0.25 \lambda - 0.162 \lambda = 0.088 \lambda$

(Smith chart is attached behind.)

Q.6(b) Find the Thevenin's equivalent across the terminals XY for the circuit shown in figure. [10]



(A)



$$i_x = \frac{V_1}{5}$$

Relation between node  $V_1$  &  $V_2$

$$V_1 - V_2 = 10 i_x$$

$$\therefore V_1 - V_2 = 10 \left( \frac{V_1}{5} \right)$$

$$V_1 - V_2 = 2V_1$$

$$V_1 + V_2 = 0$$

...(1)

Supernode equation

$$\frac{V_1}{5} + \frac{V_2}{10} = 1$$

...(2)

Solving (1) and (2)

$$V_1 = 10 \text{ V}$$

$$V_2 = -10 \text{ V}$$

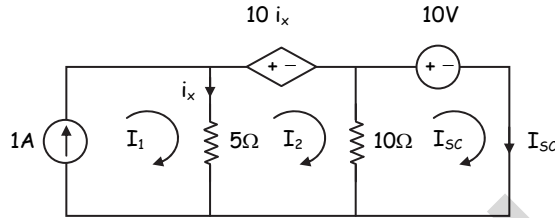
Relation between  $V_2$  &  $V_{th}$

$$V_2 - V_{th} = 10$$

$$-10 - 10 = V_{th}$$

$$\therefore V_{th} = -20 \text{ V}$$

Finding  $I_{SC}$



$$I_1 = 1 \text{ A}$$

$$i_x = I_1 - I_2 = 1 - I_2$$

...(3)

Apply KVL to  $I_2$

$$-5(I_2 - 1) - 10(1 - I_2) - 10(I_2 - I_{SC}) = 0$$

$$-5I_2 + 10I_{SC} = 5$$

...(1)

Apply KVL to  $I_{SC}$

$$-10(I_{SC} - I_2) - 10 = 0$$

$$10I_2 - 10I_{SC} = 10$$

...(2)

Solving (1) to (2)

$$I_2 = 3 \text{ A}$$

$$I_{SC} = 2 \text{ A}$$

Find  $R_{th}$

$$R_{th} = \frac{V_{th}}{I_{SC}} = \frac{|20|}{|2|} = 10\Omega$$

Thevenin's equivalent circuit is as follows

